

SI/C ELECTRODE MULTISCALE MODELLING FROM ATOMS TO CELLS WORKSHOP @ POLYTECHNIQUE SCHOOL IN PALAISEAU

MARTIN PETIT – IFP ENERGIES NOUVELLES





Next generation batteries



This project has received funding from the European Union's Horizon 2020 research and innovation program under grant agreement No 875193.

G	 90-235 Wh/kg 200-630 Wh/l 	Advanced Li-ion Gen 3b	350 Wh/kg, 750 Wh/l • 2025 ? Solid State Gen 4 • 450 Wh/kg, 1100 Wh/l • 2030 ??		
Nationale Plattfo	rm Elektromobilität, Deutschland Jan. 2016	-	New technologies relying on new materials to		
Cell generation	Cell chemistry		improve batteries performances		
Generation 5	Li/O2 (lithium-air)Conversion materials (LiS)		 Gen 3b Use of Silicon in the negative Graphite 350 mAh/g 2 + 15% vol Silicon 3000 mAh/g 2 + 300% vol Need to account for volumetric expansion 		
Generation 4	 All-solid-state batteries Gr ou Si/Gr anode (Gen 4a) Li metal (Gen 4b) 	> 2025			
Generation 3b	 Cathode: HE-NMC, High Voltage Spinnel Anode: Silicon/carbon (>20% Si) 	≈ 2025	 Long term effect on aging Cell swelling 		
Generation 3a	 Cathode: NMC 622 to 811 Anode: Silicon/carbon (5-10% Si) 		 Gen 4 Use of solid electrolyte 		
Generation 2b	Cathode: NMC 532 to 622Anode: 100% carbon		New ionic conduction typeSolid/solid interfaces		
Generation 2a	Cathode: NMC 111Anode: 100% carbon	- current	 Stability issues at the Li/electrolyte interface 		
Generation 1	Cathode: LFP or NCAAnode: 100% carbon				



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Specific needs from all stakeholders



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Si-based anode modelling toolchain



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Each scale brings information necessary for understanding and forecasting the complete cell behavior





Studied system



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- Gen 3b cell
 - NMC811
 - SiOx/C negative electrode (aim >20% Si)
 - 1M LiPF6 in EC:DMC (3:7) + 10% FEC
- Commercial negative material
 - Complex formulation needing specific characterization
 - Graphite particles: 77%
 - Si based particles
 - Si inclusion in SiO2 matrix + 20nm Graphite layer
 - Quantification Si_0/Si_{IV} : 50/50

























- Coin cells prepared with material
 - Formed
 - Capacity 580 mAh/g (theoretical 650 mAh/g)
 - Ocycled 10 times
- SEM polished section observations (not performed on lithiated electrodes)
 - Observed swelling of cycled electrode
 - Looser packing of particles
- SEM direct powder deposition
 - Heterogeneous contrast due to
 - Heterogeneous lithiation
 - Heterogeneous SEI thickness
 Isos of electric contact with collectors
 - Cracks present on SEI in cycled samples







Intrisic material properties through ab initio modelling



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- Simulation focused on intrinsic properties for the material Diffusion properties investigated through Nudged Elastic Band \bigcirc
 - methodology
 - Evaluation of hoping *a* distance between adjacence sites \bigcirc

$$D(T) = a^2 v^* \exp\left(-\frac{\Delta G^{++}}{KT}\right)$$

- ΔG^{++} Gibbs free energy of activation for ion hopping calculated by NEB v^* effective attempt frequency calculated by phonon calculations at the beginning and transition states

Case	∆G ⁺⁺ (eV)	v* (Hz)	D(cm²/s) @T=300K
ODH	0.78	3.5E+13	2.6E-15
TSH	0.56	3.2E+12	1.6E-12

- Same methodology applied in solid state electrolytes
 DFT modelling of negative electrode active materials
 Ab initio molecular dynamics \bigcirc
 - - Creation of amorphous silicon and amorphous lithium silicide models
 - Interpolation of volumetric expansion vs. Li content curve
 - Analysis of bond-breaking patterns at low and high Li contents
 - Elastic properties: \bigcirc
 - Ab-initio calculation of elastic tensor and mechanical parameters
 - Consequences of lithiation and delithiation on the chemical and mechanical properties of all anode components

Parameters can be further used in larger scale simulations \bigcirc





Lithiated anode materials







Understanding of particle behaviour



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- Study or the enect of Limisertion on particle behaviour
 - Olume variation
 - O Stress generation
 - Mechanical properties variation











Mechanical electrode scale modelling – FEM approach



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• Principle of the model :

- DEM to generate an initial assembly of particles
- Cylindrical bridges are inserted between neighbors
- In FEM, grains are dilated linearly, depending on the material
- Key element of the model : the bridges
 - Assumption the binder is concentrating at grains contact
 - Initial model with elastoplastic bridges do not converge (too much distortion)
 - Second model use cohesive zone for breakage modeling
- Many issues encountered
 - Considerable difficulties on numerical convergence (stability, damage modeling)
 - Observe and the server of t
- Switch to full DEM approach













DEM model of electrode material \bigcirc

- Si/SiOx and C particles represented as an assembly sphere
 Special bonding contact laws account for the presence of binder
 "One-way" coupling for electrochemical effect on swelling
 Particle volume as a function of SOC is provided by other models
 Particle swelling as a function of time is scripted \bigcirc
- Model variables
 - Initial density \bigcirc
 - Pressure on the anode \bigcirc
 - Binder flexibility \bigcirc
 - \bigcirc Binder dispersión
- Model output

 - Evolution of anode density/volume Binder damage at first charge (no cycling) \bigcirc
- First interesting results \bigcirc
 - Swelling behaviour
 - No observed influence of binder properties on swelling behavior Swelling seems entirely piloted by active particles topology (initial
 - density, PSD)
 - Binder damage \bigcirc

 - Key property : binder strain to breakage Binder bridges accommodate strains due to grain movement... or not

Swelling and binder damage are uncoupled !











1D model at cell level





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- Use of a simplified electrochemical \bigcirc model
- SPM-e model with blend negative \bigcirc electrode
 - Based on M. Petit, E. Calas and J. \bigcirc Bernard, J.Power Sources, 2020, 479, 228766.
 - Compatible with long term simulation for aging
 - Accounting for nominal electrochemical behaviour
 - **Electrochemical kinetics**
 - Electrolyte behavior
 - Liquid mass and charge balances
 Active material behavior
 - - Solid mass and charge balance
 - Accounting for aging phenomena \bigcirc
 - SEI layer formation on both material in \bigcirc the negative
 - Li plating

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- Loss of active material at the positive
- With mechanical aspects \bigcirc
 - Stress induced diffusion \bigcirc
 - Cracks induced SEI formation
 - Loss of active material due to mechanical stresses

mechanisms		Boundary conditions
Solid phase: conservation of Li ⁺ species	$\frac{\partial}{\partial t}c_{s}^{k} - \frac{1}{r^{2}}\frac{\partial}{\partial r}\left(r^{2}\mathcal{D}_{s}^{k}\frac{\partial}{\partial r}c_{s}^{k}\right) = 0$	$\mathcal{D}_{s}^{k} \frac{\partial}{\partial r} c_{s}^{k} \Big _{r=0} = 0$ $-\mathcal{D}_{s}^{k} \frac{\partial}{\partial r} c_{s}^{k} \Big _{r=0} = \frac{I_{elec}^{k}}{a_{s}^{k} A_{elec} \delta_{elec} F}$
Electrolyte phase: conservation of Li ⁺ species	$\frac{\partial}{\partial t}\varepsilon^e c^e - \frac{\partial}{\partial z} \left(D_e^{eff} \frac{\partial}{\partial z} c_e \right) - (1 - t^+) \frac{\sum_k j_f^k}{F} = 0$	$\frac{\partial}{\partial z} c^{e} \Big _{z=0} = \frac{\partial}{\partial z} c^{e} \Big _{z=L} = 0$
Solid phase: charge conservation	$\frac{\partial}{\partial z} \left(\sigma_{eff} \frac{\partial}{\partial z} \phi_s \right) - \sum_k j_f^k = 0$	$-\sigma_{eff}^{n} \frac{\partial}{\partial z} \phi_{s} \Big _{z=0} = -\sigma_{eff}^{p} \frac{\partial}{\partial z} \phi_{s} \Big _{z=1}$ $= I/A_{elec}$ $\frac{\partial}{\partial z} \phi_{s} \Big _{z=\delta_{n}} = \frac{\partial}{\partial z} \phi_{s} \Big _{z=L-\delta_{n}} = 0$
Electrolyte phase: charge conservation	$\frac{\partial}{\partial z} \left(\kappa_{eff} \frac{\partial}{\partial z} \phi_e \right) + \frac{\partial}{\partial z} \left(\kappa_{eff}^D \frac{\partial}{\partial z} \ln c_e \right) + \sum_k j_f^k(z) = 0$	$\frac{\partial}{\partial z}\phi_e\Big _{z=0} = \frac{\partial}{\partial z}\phi_e\Big _{z=L} = 0$
Electrochemical kinetics	$j_{f}^{i} = a_{s}^{i} i_{0}^{i} \left(exp\left(\frac{\alpha \mathcal{F}}{RT} \bar{\eta}_{ct}^{i}\right) - exp\left(-\frac{(1-\alpha)\mathcal{F}}{RT} \bar{\eta}_{ct}^{i}\right) \right)$ $j_{f}^{j} = a_{s}^{j} i_{0}^{j} \left(exp\left(\frac{\alpha \mathcal{F}}{RT} \bar{\eta}_{ct}^{j}\right) - exp\left(-\frac{(1-\alpha)\mathcal{F}}{RT} \bar{\eta}_{ct}^{j}\right) \right)$ $i_{0}^{i} = k_{0}^{i} c_{e}^{\alpha_{0,i}} \left(c_{s}^{i,max} - c_{s}^{i} (R_{n}^{i}) \right)^{\alpha_{0,i}} c_{s}^{i} (R_{n}^{i})^{\alpha_{0,i}}$ $i_{0}^{j} = k_{0}^{i} c_{e}^{\alpha_{0,i}} \left(c_{s}^{j,max} - c_{s}^{i} (R_{n}^{i}) \right)^{\alpha_{0,i}} c_{s}^{j} (R_{n}^{i})^{\alpha_{0,i}}$	
Electrode overpotential	$ \begin{aligned} \vec{v}_0 &= \vec{k}_0 c_e^{-1} \left(c_s^{c} - c_s^{c} (\vec{k}_p) \right) \\ \bar{\eta}_c^{k} &= \Delta \phi - U_{elec}^{k} = \overline{\phi_s} - \overline{\phi_e} - U_{elec}^{k} \end{aligned} $	
Double layer capacity	$\frac{d\Delta\phi_p}{dt} = \frac{1}{a_s^p A_{elec} \delta_p C_{dl}^p} \left(I - A_{elec} \int_{L-\delta_p}^{L} \sum_j j_f^j dz \right)$ $\frac{d\Delta\phi_n}{dt} = \frac{1}{a_s^n A_{elec} \delta_n C_{dl}^n} \left(-I - A_{elec} \int_0^{\delta_n} \sum_i j_f^i dz \right)$	
Electrolyte ionic diffusional conductivity	$\kappa_{eff}^{D} = \frac{2RT\kappa_{eff}}{\mathcal{F}}(t_{+} - 1)\left(1 + \frac{d\ln f_{\pm}}{d\ln c_{e}}\right)$	
Solid phase electronic conductivity	$\sigma_{eff} = \frac{\sum_{k} \varepsilon_{s}^{k} \sigma_{k}}{\sum_{k} \varepsilon_{s}^{k}}$	

 $I\delta_{elec}$

 $3A_{elec}\sigma_{ef}$

 $\eta_s = \frac{1}{2}$



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Solid phase overvoltage



• Main assumption:

- Cell behave like a spring
 - Material swelling cause displacement
 - Other materials (packaging, separator...) have stiffness
- Following results from DEM
 - Active material volumetric change = whole electrode volumetric change
- Evaluation of a displacement due to volume variation

$$\frac{ll_{cell}}{dt} = \frac{N_{stack}}{A_{elec}} \sum \frac{dV_{s_i}}{dt}$$

Over the second seco

$$\frac{dV_{s_i}}{dt} = \frac{\varepsilon_s^i l_{elec}^0}{c_s^{max}} \left(\frac{dc_s^i}{dt} \beta \left(\overline{c_s^i} \right) + \overline{c_s^i} \frac{d\beta}{dt} \bigg|_{\overline{c_s^i}} \right)$$

• β is the volumetric expansion coefficient (different for Si and Graphite)





Model outputs



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- Classical cell behaviour \bigcirc
 - Voltage \bigcirc
 - Heat release \bigcirc
 - Swelling \bigcirc
 - From DEM calculation \bigcirc
 - Cell length change given by material volume change
 - \bigcirc
- 2 steps during discharge
 Gr deintercalation low volumetric change
 - Si deintercalation with high volumetric change \bigcirc
- Accessible variables \bigcirc
 - Material concentrations
 - Current repartition between materials \bigcirc
 - Potentials

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Energies nouvelles







Modelling of aging phenomena



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- SEI formation
 - Simplified SEI formation formulation without SEI convection
 - SEI formation current computed
 - Leading to Loss of Li inventory
 - SEI thickness increase
- Li plating
 - O Reversible Li plating
 - Lithium trapping into inactive materials I dead Li
- Loss of positive active material
 - Oxidation of positive active material leading to loss of active material
- Cracks induced SEI formation
 - Based on stresses computed in particles

$$\frac{dA_{cr}}{dt} = k_{cr} \frac{d\sigma_{\theta}|_{r=R_n}}{dt}$$

- Increased SEI formation rate with no SEI thickness incease
- Cracks induced LAM
 - Based on stress calculated in model $\frac{dC_{loss}}{dt} = \beta_{mec} \max_{r} \left| \frac{d\sigma_{\theta}(r)}{dt} \right|$
 - Or based on contact losses computed in DEM I loss of active material

•
$$\frac{d\Delta\varepsilon}{dt} = k_{LAM} \frac{dC_{loss}}{dt} \Big|_{SOC}$$



Charge balance leading to loss of Li inventory

$$\begin{split} I_{neg} &= I_{gr} + I_{SiOx} + I_{SEI} + I_{pl} \\ I_{pos} &= I_{NMC} + I_{ox} \\ \text{Impact of loss of active material} \\ \varepsilon^{s}_{neg} &= \varepsilon^{s}_{neg}_{0} (1 - \Delta \varepsilon_{LAM}) \\ \varepsilon^{s}_{pos} &= \varepsilon^{s}_{pos}_{0} (1 - \Sigma \Delta \varepsilon_{LAM}) \end{split}$$





Evaluation of cell formation



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- Aim simulate a realistic formation cycle
 - Pristine electrode are set-up in the model
 - Fully lithiated NMC in the positive
 - Empty negative electrode
 - Formation cycle used for real MODALIS² cells
 - O Design taken from Saft
 - Model operates as a test bench and automatically switch between rest, CC and CV
- 41 h simulated in 10 minutes
- Initial cell capacity computed
 - 5,58 Ah VS 5,63 as mean capacity for manufactured cells









OC/CV cycles simulated

- From initial formation starting point
- Fast simulation (7 parallel runs)
 - 400 000 s simulated (36 full DoD cycles)
 - 3 000 s computational time
 - 800 000 s simulated (57 full DoD cycles)
 - 4300 s computational time
- Evaluation of the effect of each aging phenomenon
- Cycle:
 - CC at 6A or 3 A then CV at 4,2 V
 - O CC at -6 A until 2,7 V
 - Cell capacity evaluated at 6A during discharge
- Main aging phenomena (qualitatively)
 - LAM due to stresses
 - O Then SEI with visible impact of cracking







3D cell modelling – non-uniform aging





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 Non-uniform aging in thermo-electro-chemically coupled macrohomogenous model (P2D) with realistic geometry







ntercalation Particle Inactive Volume Fraction of Graphit

Heterogeneous SEI formation

Intercalation Particle Surface Film Thickness of SEI (m) 1.05e-08 1.25e-08 1.45e-08







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Heterogeneous loss of Active materials

Conclusions and perspectives



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- Full toolchain implemented for Gen3b cells
 - Link between material electrode full cell behaviour
 - Phenomena studied
 - Mechanical behaviour
 - Diffusion
 - Aging
 - Thermal stability
- Tool chain to be validated against experimental data
 - Extensive aging campaign
 - Oedicated devices to evaluate swelling
- MODALIS² ongoing developments to focus on Gen4 cells
 - Solid electrolyes with metal Li
 - O Development initiated on argyrodite behaviour
 - Li conductivity
 - Chemical stability
 - 1 D model to be adapted to account for Li electrode











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2 mAh / 0,4 cm²

High operating pressure (>100 MPa)

Further development in IFPEN



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- Current PhD thesis supervised by Eric Maire (INSA Lyon Mateis)
 - Abhilash Valisammagari
 - Combined experimental/modelling assessment of Si based anode materials for Li-ion batteries
 - Use of DEM Swelling behavior
 - Implement complex particle shape (graphite platelet, angularity)
 - Key to any truly predictive work on density
 - Optimize the density you get after cycling, not after calendering
 - Density evolves heavily due to particle rearrangement
 - Binder damage
 - Link between binder topology and mechanics
 - Where do we have binder ? How much ? In which configuration ?
 - Introduce realistic binder properties to assess cycling behavior
 - Irreversible strain and fatigue, binder recovery
 - Experimental investigation of electrode behavior
 - In situ CT-XRD to evaluate electrode swelling
 - ESRF time slot in January to observe binder behavior in situ
- AURANODE project
 - Use of other type of Si based particles with lower volume variation at particle scale
 - Need of dedicated particle scale modelling















THANKS A LOT FOR YOUR ATTENTION

HTTPS://MODALIS2-PROJECT.EU/

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